Corrigenda to the **Ignition Handbook**

Page 10, 1st col., 3rd par.
Original:
The failure rate has been estimated as 2×10^{-6}/year, as based on an estimated 1.62 billion outlets that are in use and are carrying current.
Corrected:
The failure rate of electrical outlets has been estimated as 2×10^{-6}/year, as based on an estimated 1.62 billion outlets that are in use and are carrying current.

Page 31, 2nd col., 7th line
Original:
hydrogen, and hydrogen are exceptions
Corrected:
hydrogen, and hydrogen sulfide are exceptions

Page 261, first equation
Original:
$$h_c = 6.56 \cdot \dot{q}_e''^{0.35}$$
Corrected:
$$h_c = 6.56\times10^{-3} \cdot \dot{q}_e''^{0.35}$$

Page 535, Figure 26
Y-axis should not have the words "peak-to-peak"

Page 536, Figure 28
X-axis label should read Volts (rms)

Page 544, 1st col., 7th par.
Original:
The power density
Corrected:
The enthalpy density

Page 569, Figure 59
Time scale should be "ms", not "s"

Page 568, 2nd col., 2nd par.
Delete sentence starting with "The power dissipated

Page 651, Color Plate 57 caption
Original:
Cut-away view of sacrificial TCOs—upper TCO closed, lower TCO open.
Corrected:
Cut-away view of sacrificial TCOs—lower TCO closed, upper TCO open.

Page 832, 1st col., last par.
Original:
The minimum flux[1102] for vertically oriented vinyl-asbestos tile of unspecified thickness was found to be 38 kW m^{-2} for autoignition and 72 kW m^{-2} for piloted ignition.

Corrected:
The minimum flux[1102] for vertically oriented vinyl-asbestos tile of unspecified thickness was found to be 72 kW m^{-2} for autoignition and 38 kW m^{-2} for piloted ignition.

Page 852, 1st col., last par.
Original:
In temperate climates, explosions have been known to occur while emptying a container. The process of emptying the liquid pulls air into the container and a region within the container can get created that is below the UFL.
Corrected:
It has been claimed that explosions can occur in temperate climates while emptying a container, due to entry of ambient air into the container. This is not supported by the published literature. There have been no case histories published where an event of this kind would have been documented. In addition, there have been no experiments that would support this suggestion; instead, experimental work has shown the opposite, that containers will not explode (J. D. DeHaan, Kirk's Fire Investigation, 6th ed., Pearson Education, 2006, pp. 70-71).

Page 955, Table 219
Correction:
Table 219, the "high pressure steam pipe" line should contain the footnote: *This incident does not comprise low-temperature, long-term heating but is included here to present the entire table published by the original authors.

Page 1057
The MIE value for gasoline is 0.24 mJ (not 0.8)

Corrigenda to the **Ignition Handbook Database**

The MIE value for gasoline is 0.24 mJ (not 0.8)

The final portion of Table 15 (p. 1070 in the book) has been omitted from "4 – Solids – Ignition temperatures"

PVC, flexible	250-280	
	422	424
PVC, flexible, wire-insulation grade		263
PVC, rigid	360 – 430	480-550
		502
PVC, rigid, FR		571
PVC floor tiles	370-410	
PVC foam, flexible	441	441
SAN (styrene/acrylonitrile copolymer)	366	454
		542
	329	485
SBR (styrene-butadiene rubber)	360	450
silicone, w. glass reinforcement	490-527	550-564
urea formaldehyde		540
		630
vinyl asbestos	431	434
vinyl epoxy adhesive	333	414
XLPE (crosslinked polyethylene)	374	427
XLPE , FR	352	383